F<del>II</del>(

ACTA TECHNICA CORVINIENSIS - Bulletin of Engineering Tome VI (Year 2013) - FASCICULE 2 [April-June] ISSN 2067-3809



<sup>1.</sup> Cristina HORA, <sup>2.</sup> Simona DZIȚAC, <sup>3.</sup> Călin SECUI, <sup>4.</sup> Gabriel BENDEA

## RELIABILITY ANALYSIS OF SPHERICAL VALVE (VS) FROM HPP REMEȚI USING MONTE CARLO SIMULATION

<sup>1-4.</sup> University of Oradea, Faculty of Power Engineering and Industrial Management, 1, Universității, Oradea, ROMANIA

ABSTRACT: In every hydro energetic arrangement, the water approaches, in differently construction elements and trough them, are equipped with valves. These valves assure the normal functioning of equipments, respectively there operatively insulation in case of failures or repairs. Also, the reliability level of hydro mechanical equipments can have a major impact on the operational reliability of HPP (Hydro Power Plants). In consequence, there are justified the concerns regarding the predictive reliability of them. In this paper, these studies of hydro-mechanical equipments reliability are made using the Monte Carlo simulation. KEYWORDS: reliability, hydro mechanical equipment, Monte Carlo simulation

## INTRODUCTION

In every hydro energetic arrangement, the water approaches, in differently construction elements and trough them, are equipped with valves. These valves assure the normal functioning of equipments, respectively there operatively insulation in case of failures or repairs.

The accomplished studies [4, 5], indicate that some valves type are more performing under the reliability aspects than other equipments (hydraulic turbines). In succession, on the reliability studies, the valves are treated as bivalent elements (Functioning; Faulting).

The reliability analysis of hydro mechanical equipments it has been made using the Monte Carlo simulation [2, 6, 7].

RELIABILITY ANALYSIS OF SPHERICAL VALVE (VS) FROM HPP REMETI USING SIMULATION PROGRAM

The spherical valve equipment, SV 150-500, is a complex ensemble who attended the hydraulic turbine FVM 52-320. It is located upstream of turbine and downstream of distributor. The spherical valve performed one's functions namely, the safety device for turbine.

The valve control its automatic realize, in the hydro generator on-off process. During a several distinctly operations the spherical valve it has manual control, from the local panel.

During the reliability analyses, the spherical valve (SV) from HPP Remeti, it has been regarded like a system compound of following subsystems (figure 1):

The closing subsystem (CSS);

The sealing subsystem (SSS);

The control subsystem (NSS);

The operate subsystem (OSS); The protection subsystem (PSS).

Figure 1. The spherical valve subsystems According to previously specifications (for the simplified reliability analyses) SV it has been treated as a system compound of five subsystems. In consequence, it can represent the simplified equivalent diagram, who reflects the necessity that, all the subsystems to be in work for satisfied all the spherical valve functions.



Figure 2. The equivalent diagram of SV

Depend on results obtained from the operational reliability studies [4,5], it can estimate the subsystems reliability indicators  $[R_i, Fi, \mu_i, M_i]$ .

## ACTA TECHNICA CORVINIENSIS – Bulletin of Engineering

The calculus relations are:

$$F_{SV} = \frac{\lambda}{\lambda + \mu}; F_i = \frac{v_i [\%]}{100} F_{SV};$$
  

$$\mu_i = \frac{v_i [\%]}{\beta_i [\%]} \mu; M_i = 1 - e^{-\mu_i - t_r}$$
(1)

where:  $\lambda$ ,  $\mu$  - the SV reliability indicators;  $F_{SV}$  - failure probability of SV;  $v_i$ ,  $B_i$  - the weight of number failures and failures

time, of the (i) subsystems from the total value of these indicators at the level of SV.

The maintainability values  $(M_i)$  are determined using condition that the maintenance corrective operations must finished in MTM = 42 h [4]. The values are represented in table 1.

Table 1 - The values of reliability indicators for the VS subsystems

Subsystem	CSS (E1)	SSS	(E2)	NSS (E3)
$F_i \times 10^3$	3.9355	27.7	7062	9.2878
$\mu_i h^{-1}$	0.00625	0.00	0855	0.006
-M <sub>i</sub>	0.23087	0.30	0169	0.22282
R <sub>i</sub>	0.9960645	0.972	22938	0.9907122
$\lambda_i [h^{-1}]$	0.000024694	0.000	24363	0.000056249
Subsystem	OSS (E4)			PSS (E5)
$F_{i} \times 10^{3}$	101.852			14.6402
$\mu_i h^{-1}$	0.006908	1		0.007159
M <sub>i</sub>	0.251838	1	(	.2596838
$R_i$	0.898148		0	0.9853598

These values will be input into the simulation program whose editing window is shown in figure 3.

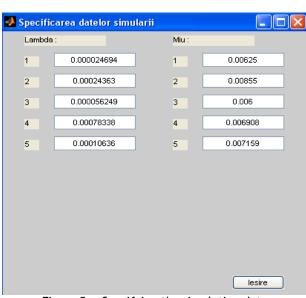
🛃 Specificarea datelor simularii 🔳 🗖 🔀
Specificare sistem
Specificare parametrii lambda si mu
O how data
Salvare date
Incarcare date
lesire

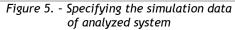
Figure 3. - The editing window of analyzed system

Following the steps from [2, 3], it's obtained figures 4÷7, which refers to the characteristic equation, specifying the input data, the failure and repair rate values, also the saved and loading data windows of simulated system.

<b>3</b>	Specificarea sistemului simulat	
	Ecuatia caracteristica a sistemului echivalent	
	E1&E2&E3&E4&	E5
		lesire

Figure 4. - The characteristic equation of system

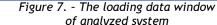




Salvare date	e	· · · · · · · · · · · · · · · · · · ·
Save in: 🔀	Program de simulare	
CENTRALA     Centrala 7.     Centrala 7.     CHE REME     CHE Tileag     CHE TILEA     CRINA.ma	mat TI.mat d.mat GD_1.mat	DIANA.mat     FINALT.mat     MECANICA.mat     ORADEA NORD.mat     sistem 8 elemente final.mat     sistem 8 elemente.mat
<		>
File name:	Subsystem	Save
Save as type:	MAT-files (*.mat)	Cancel

Figure 6. -The saved data window for system analysis

Incarcare date	? 🛛
Look in: 🗀 Program de simulare	- 🖬 🍋 🛋
CENTRALA 4.mat Centrala 7.mat CHE REMETI.mat CHE Tileagd.mat CHE TILEAGD_1.mat CHE TILEAGD_1.mat CRINA.mat	DIANA.mat  FINALT.mat  MECANICA.mat  ORADEA NORD.mat  Sistem 8 elemente final.mat  sistem 8 elemente.mat
	>
File name: Subsystem.mat	Open
Files of type: MAT-files (*.mat)	▼ Cancel



📣 Simulare	
Timpul de simulare	
15	
Numarul de simulari	
10000	]
Simulare	]
	lesire
The strend stiens as a de	1 . 6 45

Figure 8. - The simulation module for 15 years and 10 000 simulations

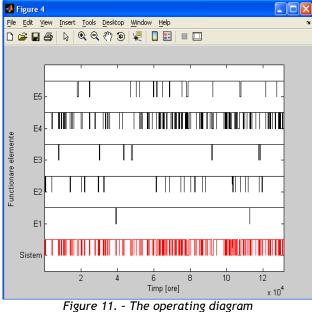
Figure 8 shows how to display the results for 15 years of analysis and 10.000 simulations, so that in figure 9 is presented the simulation results display window.

Rezultate simula	are
Perioada de simular	re T_A :15 ani.
Durata de functiona	are/an (alfa) :7453.3483 ore.
Durata de functiona	are pe perioada T_A :111800.2246 ore.
Durata de nefunctio	onare/an (beta) :1306.6517 ore.
Durata de nefunctio	onare pe perioada T_A :19599.7754 ore.
Numar de intrerupe	ri/an [niu] :8.9048 intreruperi.
Numar de intrerupe	ri pe perioada T_A :133.5714 intreruperi.
MTBF	:837.0072
МТМ	:146.7363
Lambda sistem	:0.0011947
Miu sistem	:0.0068149
R sistem	:0.85084
F sistem	:0.14916
Salvare rez.	

Figure 9. - The simulation results display window

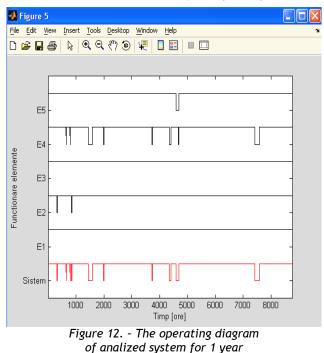


Figure 10. - The window display module of operating diagram for analysis system



of analyzed system for 15 years

Figure 10 shows the display module of operating diagrams and diagram in figure 11, 12 presents the corresponding data input module. It is noted the existence of defects over time at both component and system level. This and the simulation results are due to the elements in series of analyzed system.



To be convinced of the usefulness and accuracy of the reliability simulation program will be a comparison of the results obtained by simulation and those obtained by analytical calculus - DEF method - [4,5], on reliability.

The analytical calculus of system reliability is  $R_{sis} = 0.849132$ , comparable to that obtained in the simulation, which was:  $R_{sis} = 0.85084$ .

Must be made clear that the simulation results are influenced by the system evolution in time, taking into account the defects that occur during the analysis. It is observed that defects are the most common at element 4 which has the lowest reliability. Frequent defects of 4 element, serially connected to the other element, leading to overall system failure, so to decrease system reliability.

It is found that the differences that arise in calculating the reliability by Monte Carlo and analytical methods are very small, which gives the judge that Monte Carlo simulation method can be applied in reliability analysis of hydraulic equipment. CONCLUSIONS

- 1. In the reliability analysis will consider the spherical valve (VS) as a complex system consists of five subsystems connected in series.
- 2. For complex systems, the program presented in [2] and run for VS is considered very effective, allowing reliability calculus, drawing of operating diagrams for all elements and system in record time.
- 3. The assessments made by this program are accurate, these results derived comparing the reliability by Monte Carlo simulation, or directly through DEF.

## ACTA TECHNICA CORVINIENSIS – Bulletin of Engineering

System	MONTE CARLO 10000 simulations	DEF
VS	<i>R<sub>sis</sub></i> = 0.849132	$R_{sis} = 0.85084$

- 4. The Monte Carlo method remains one of the successful methods in various energy analysis. REFERENCES
- [1.] Felea, I. Ingineria fiabilității în electroenergetică, Editura Didactică și Pedagogică, București, 1996
- [2.] Dziţac, S. Fiabilitatea şi disponibilitatea sistemelor de distribuţie a energiei electrice, Editura Universităţii din Oradea, ISBN: 978-973 -759 -754 - 0, 2009
- [3.] Dziţac Simona, Vesselenyi T., Dziţac I., Văleanu E., Electrical power station reliabilitymodelling procedure using the Monte Carlo method, The 4 th International Federationof Automatic Control Conference on Management and Control of Production and Logistics IFAC MCPL, 27-30 septembre, 2007, Sibiu, România, vol III, pp. 695-700, ISBN: 978-973-739-481-1, Papers published by Elsevier (Pergamon)

- [4.] Hora, C. Fiabilitatea echipamentelor din centralele hidrolectrice, Editura Universității din Oradea, 2007
- [5.] Hora, C., Vereş, M. Contributions regarding the predictive reliability analysis of the hydro mechanical equipments from hydro power plants, The 6<sup>th</sup> International Conference on Electromechanical and Power Systems, SIELMEN 2007, 4-6 octombrie, Chişinău
- [6.] Hora C., Dziţac S., Dumitrescu D., Hora H. -Reliability analysis of cut-off plate (vir) from HPP Tileagd using Monte Carlo simulation Journal of Sustainable Energy, vol. II, No. 1, March, 2011, pg. 21-25, ISSN 2067-5534
- [7.] Hora C., Dziţac S., Dumitrescu D., Hora H., Reliability analysis of hydro - generator groups using Monte Carlo simulation Annals of the Oradea University, Fascicle of Management and Technological Engineering, volume X(XX), 2011, nr. 2, pg. 24-29, ISSN 1583-0691



ACTA TECHNICA CORVINIENSIS - BULLETIN of ENGINEERING



ISSN: 2067-3809 [CD-Rom, online]

copyright © UNIVERSITY POLITEHNICA TIMISOARA, FACULTY OF ENGINEERING HUNEDOARA, 5, REVOLUTIEI, 331128, HUNEDOARA, ROMANIA <u>http://acta.fih.upt.ro</u>